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In: Jan Chleboun and Petr Přikryl and Karel Segeth and Jakub Šístek (eds.): Programs and Algorithms of Numerical Mathematics, Proceedings of Seminar. Dolní Maxov, June 6-11, 2010. Institute of Mathematics AS CR, Prague, 2010. pp. 35–41.

Persistent URL: http://dml.cz/dmlcz/702738

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### INTERACTION OF COMPRESSIBLE FLOW WITH AN AIRFOIL\*

Jan Cesenek, Miloslav Feistauer

#### Abstract

The paper is concerned with the numerical solution of interaction of compressible flow and a vibrating airfoil with two degrees of freedom, which can rotate around an elastic axis and oscillate in the vertical direction. Compressible flow is described by the Navier-Stokes equations written in the ALE form. This system is discretized by the semi-implicit discontinuous Galerkin finite element method (DGFEM) and coupled with the solution of ordinary differential equations describing the airfoil motion. Computational results showing the flow induced airfoil vibrations are presented.

#### 1 Formulation of the continuous problem

We consider 2D compressible viscous flow in a bounded domain  $\Omega(t) \subset R^2$  depending on time  $t \in [0, T]$ . We assume that the boundary  $\partial \Omega(t)$  of  $\Omega(t)$  consists of three disjoint parts:  $\partial \Omega(t) = \Gamma_I \cup \Gamma_O \cup \Gamma_W(t)$ , where  $\Gamma_I$  is inlet,  $\Gamma_O$  is outlet and  $\Gamma_W(t)$  is impermeable wall, whose part may move.

The time dependence of the domain is taken into account with the aid of a regular one-to-one ALE mapping (cf. [4])  $\mathcal{A}_t : \Omega_0 \longrightarrow \Omega_t$ , i.e.  $\mathcal{A}_t : X \longmapsto x = x(X,t) = \mathcal{A}_t(X)$ . We define the ALE velocity  $\tilde{\boldsymbol{z}}(X,t) = \partial \mathcal{A}_t(X)/\partial t$ ,  $\boldsymbol{z}(x,t) = \tilde{\boldsymbol{z}}(\mathcal{A}^{-1}(x),t)$ ,  $t \in [0,T]$ ,  $X \in \Omega_0$ ,  $x \in \Omega_t$ , and the ALE derivative of a function f = f(x,t) defined for  $x \in \Omega_t$  and  $t \in (0,T)$ :  $D^A f(x,t)/Dt = \partial \tilde{f}(X,t)/\partial t$ , where  $\tilde{f}(X,t) = f(\mathcal{A}_t(X),t)$ ,  $X \in \Omega_0$ .

$$\frac{D^{A}\boldsymbol{w}}{Dt} + \sum_{s=1}^{2} \frac{\partial \boldsymbol{g}_{s}(\boldsymbol{w})}{\partial x_{s}} + \boldsymbol{w} \operatorname{div} \boldsymbol{z} = \sum_{s=1}^{2} \frac{\partial \boldsymbol{R}_{s}(\boldsymbol{w}, \nabla \boldsymbol{w})}{\partial x_{s}}, \qquad (1)$$

where for i, j = 1, 2 we have

$$\boldsymbol{w} = (w_1, \dots, w_4)^T = (\rho, \rho v_1, \rho v_2, E)^T \in \mathbb{R}^4, \quad \boldsymbol{g}_i(\boldsymbol{w}) = \boldsymbol{f}_i(\boldsymbol{w}) - z_i \boldsymbol{w}, \qquad (2)$$
  
$$\boldsymbol{f}_i(\boldsymbol{w}) = (f_{i1}, \dots, f_{i4})^T = (\rho v_i, \rho v_1 v_i + \delta_{1i} p, \rho v_2 v_i + \delta_{2i} p, (E+p) v_i)^T, \qquad (2)$$
  
$$\boldsymbol{R}_i(\boldsymbol{w}, \nabla \boldsymbol{w}) = (R_{i1}, \dots, R_{i4})^T = (0, \tau_{i1}^V, \tau_{i2}^V, \tau_{i1}^V v_1 + \tau_{i2}^V v_2 + k\partial\theta/\partial x_i)^T, \qquad \tau_{ij}^V = (-2\operatorname{div} \boldsymbol{v}/3 \, \delta_{ij} + 2 \, d_{ij}(\boldsymbol{v}))/Re, \quad d_{ij}(\boldsymbol{v}) = (\partial v_i/\partial x_j + \partial v_j/\partial x_i)/2.$$

<sup>\*</sup>The research of J. Česenek was supported by the Grant No. 12810 of the Grant Agency of the Charles University Prague. The research of M. Feistauer is a part of the research project MSM 0021620839 of the Ministry of Education of the Czech Republic. It was also partly supported by the grant No. 201/08/0012 of the Czech Science Foundation.

We use the following notation:  $\rho$  - density, p - pressure, E - total energy,  $\boldsymbol{v} = (v_1, v_2)$  - velocity,  $\theta$  - absolute temperature,  $\gamma > 1$  - Poisson adiabatic constant,  $c_v > 0$  - specific heat at constant volume, Re - the Reynolds number, k - heat conduction. The vector-valued function  $\boldsymbol{w}$  is called the state vector, the functions  $\boldsymbol{f}_i$  are the so-called inviscid fluxes and  $\boldsymbol{R}_i$  represent viscous terms. The above system is completed by the thermodynamical relations

$$p = (\gamma - 1)(E - \rho |\mathbf{v}|^2/2), \ \theta = (E/\rho - |\mathbf{v}|^2/2)/c_v$$

and equipped with the initial condition  $\boldsymbol{w}(x,0) = \boldsymbol{w}^0(x), x \in \Omega_0$ , and the following boundary conditions:

$$\begin{split} \rho &= \rho_D, \ \boldsymbol{v} = \boldsymbol{v}_D, \ \sum_{i,j=1}^{I} \tau_{ij}^V n_i v_j + k \frac{\partial \theta}{\partial n} = 0 \ \text{ on } \Gamma_I, \\ \boldsymbol{v}|_{\Gamma_{W_t}} &= \boldsymbol{z}_D \ - \ \text{velocity of a moving wall}, \ \partial \theta / \partial n = 0 \ \text{on } \Gamma_{W_t}, \\ \sum_{i=1}^{2} \tau_{ij}^V n_i = 0, \ j = 1, \ 2, \ \partial \theta / \partial n = 0 \ \text{on} \Gamma_O, \end{split}$$

with given data  $\boldsymbol{w}^{0}, \rho_{D}, \boldsymbol{v}_{D}, \boldsymbol{z}_{D}$ .

The terms  $\boldsymbol{R}_s$  and  $\boldsymbol{f}_s$  satisfy the relations

$$\boldsymbol{R}_{s}(\boldsymbol{w},\nabla\boldsymbol{w}) = \sum_{k=1}^{2} \mathbf{K}_{s,k}(\boldsymbol{w}) \frac{\partial \boldsymbol{w}}{\partial x_{k}}, \quad \boldsymbol{f}_{s}(\boldsymbol{w}) = \mathbf{A}_{s}(\boldsymbol{w})\boldsymbol{w}, \quad (3)$$

where  $\mathbf{K}_{s,k}(\boldsymbol{w}) \in \mathbb{R}^{4 \times 4}$  and  $\mathbf{A}_s$  is the Jacobian matrix of  $\boldsymbol{f}_s$ .

## 2 Discretization

### 2.1 Discontinuous Galerkin space discretization

By  $\Omega_h(t)$  we denote polygonal approximation of the domain  $\Omega(t)$ . Let  $\mathcal{T}_h(t) = \{K_i\}_{i \in I(t)}$  be a triangulation of the domain  $\Omega_h(t)$  formed by a finite number of closed triangles  $K_i$  with mutually disjoint interiors. We set  $h_K = diam(K)$  as the diameter of K,  $h(t) = \max_{K \in \mathcal{T}_h(t)} h_K$ , |K| is the Lebesgue measure of K. All elements of  $\mathcal{T}_h(t) = \{K_i\}_{i \in I(t)}$  will be numbered so that  $I(t) \subset Z^+ = \{0, 1, 2, 3, ...\}$  is a suitable index set. If two elements have a common face, than we call them neighbours and put  $\Gamma_{ij} = \Gamma_{ji} = \partial K_i \cap \partial K_j$ . For each  $i \in I(t)$  we define the index set  $s(i)(t) = \{j \in I(t); K_j \text{ is a neighbour of } K_i\}$ . The boundary  $\partial \Omega_h(t)$  is formed by a finite number of sides of elements  $K_i$  adjacent to  $\partial \Omega_h(t)$ . We denote all these boundary sides by  $S_j$ , where  $j \in I_b(t) \subset Z^- = \{-1, -2, -3, ...\}$  and set  $\gamma(i)(t) = \{j \in I_b(t); S_j \text{ is a side of } K_i\}, \Gamma_{ij} = S_j$  for  $K_i \in \mathcal{T}_h(t)$  such that  $S_j \subset \partial K_i, j \in I_b(t)$ . For an element  $K_i$ , not containing any boundary side  $S_j$ , we set  $\gamma(i)(t) = \emptyset$ . Obviously  $s(i)(t) \cap \gamma(i)(t) = \emptyset$  for all  $i \in I(t)$ . Moreover we define  $S(i)(t) = s(i)(t) \cup \gamma(i)(t)$ .

We shall look for an approximate solution of the problem in the space  $\mathbf{S}_h(t) = \{v; v \mid_K \in P^r(K), \forall K \in \mathcal{T}_h(t)\}^4$ , where  $r \ge 0$  is an integer and  $P^r(K)$  is the space

of polynomials of degree at most r on K. If  $v \in \mathbf{S}$ , then we use the notation  $v|_{\Gamma_{ij}}$ and  $v|_{\Gamma_{ji}}$  for the traces of v on  $\Gamma_{ij}$  from the side of the adjacent elements  $K_i$  and  $K_j$ , respectively,  $\langle v \rangle_{\Gamma_{ij}}$  for the average of traces of v on the face  $\Gamma_{ij}$  from the side of the adjacent elements and  $[v]_{\Gamma_{ij}}$  the jump of v on  $\Gamma_{ij}$ . By  $\mathbf{n}_{ij}$  we denote the unit outer normal to the boundary of  $K_i$  on  $\Gamma_{ij}$ .

For arbitrary  $t \in [0, T]$  we can multiply the system by a test function  $\varphi \in \mathbf{S}_h(t)$  integrate and sum over all  $K_i \in \mathcal{T}_h(t)$ , apply Green's theorem and introduce a numerical flux **H**. Then we introduce the following forms (cf. [1]):

$$\begin{split} \tilde{b}_{h}(\boldsymbol{w},\boldsymbol{\varphi}_{h}) &= -\sum_{i \in I(t)} \int_{K_{i}} \sum_{s=1}^{2} \boldsymbol{g}_{s}(\boldsymbol{w}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{s}} \mathrm{d}x + \sum_{i \in I(t)} \sum_{i \in S(i)(t)} \int_{\Gamma_{ij}} \mathbf{H}(\boldsymbol{w}|_{\Gamma_{ij}},\boldsymbol{w}|_{\Gamma_{ji}},\boldsymbol{n}_{ij}) \mathrm{d}S \\ \tilde{a}_{h}(\boldsymbol{w},\boldsymbol{\varphi}_{h}) &= -\sum_{i \in I(t)} \int_{K_{i}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{s,k}(\boldsymbol{w}) \frac{\partial \boldsymbol{w}}{\partial x_{k}} \cdot \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{s}} \mathrm{d}x \\ &+ \sum_{i \in I(t)} \sum_{j \in s(i)(t)} \int_{\Gamma_{ij}} \sum_{s=1}^{2} \left\langle \sum_{k=1}^{2} \mathbf{K}_{s,k}(\boldsymbol{w}) \frac{\partial \boldsymbol{w}}{\partial x_{k}} \right\rangle (n_{ij})_{s} \cdot [\boldsymbol{\varphi}_{h}] \mathrm{d}S \\ &+ \sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{ij}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{s,k}(\boldsymbol{w}) \frac{\partial \boldsymbol{w}}{\partial x_{k}} \right\rangle (n_{ij})_{s} \cdot [\boldsymbol{\varphi}_{h}] \mathrm{d}S \\ &+ \Theta \sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{ij}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{s,k}(\boldsymbol{w}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}} \right\rangle (n_{ij})_{s} \cdot [\boldsymbol{w}] \mathrm{d}S \\ &+ \Theta \sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{ij}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{k,s}^{T}(\boldsymbol{w}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}} \right\rangle (n_{ij})_{s} \cdot [\boldsymbol{w}] \mathrm{d}S \\ &+ \Theta \sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{ij}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{k,s}^{T}(\boldsymbol{w}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}} (n_{ij})_{s} \cdot \boldsymbol{w} \mathrm{d}S \\ &+ \Theta \sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{ij}} \sigma[\boldsymbol{w}] \cdot [\boldsymbol{\varphi}_{h}] \mathrm{d}S + \sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{ij}} \sigma \boldsymbol{w} \cdot \boldsymbol{\varphi}_{h} \mathrm{d}S \\ \tilde{l}_{h}(\boldsymbol{w}, \boldsymbol{\varphi}_{h}) = \Theta \sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{ij}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{k,s}^{T}(\boldsymbol{w}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}} (n_{ij})_{s} \cdot \boldsymbol{w}_{B} \mathrm{d}S \\ &+ \sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{ij}} \sigma \boldsymbol{w}_{B} \cdot \boldsymbol{\varphi}_{h} \mathrm{d}S, \end{split}$$

where  $\sigma |_{\Gamma_{ij}} = \frac{C_W}{h(\Gamma_{ij})Re}$ ,  $C_W > 0$  is a suitable sufficiently large constants and  $\boldsymbol{w}_B$  is a boundary state defined by the Dirichlet boundary condition and extrapolation. By  $(\cdot, \cdot)$  we denote the  $L^2(\Omega(t_{k+1}))$ -scalar product. We set  $\Theta = -1$  or 0 or 1 and get the so-called nonsymmetric or incomplete or symmetric version of the viscous form. In practical computations we use  $\Theta = 1$ . Now we can define the discrete problem: Find  $\boldsymbol{w}_h(t) \in \mathbf{S}_h(t)$  such that

$$\begin{pmatrix} D^{\mathcal{A}}\boldsymbol{w}_{h}(t) \\ Dt \end{pmatrix} - (\operatorname{div}\boldsymbol{z}(t)\boldsymbol{w}_{h}(t),\boldsymbol{\varphi}_{h}) + \tilde{b}_{h}(\boldsymbol{w}_{h}(t),\boldsymbol{\varphi}_{h}) + \tilde{a}_{h}(\boldsymbol{w}_{h}(t),\boldsymbol{\varphi}_{h}) \\ + J_{h}^{\sigma}(\boldsymbol{w}_{h}(t),\boldsymbol{\varphi}_{h}) = \tilde{l}_{h}(\boldsymbol{\varphi}_{h}) \quad \forall \boldsymbol{\varphi}_{h} \in \mathbf{S}_{h}(t), \quad \forall t \in (0,T), \\ \boldsymbol{w}_{h}(0) = \boldsymbol{w}_{h}^{0}.$$

where  $\boldsymbol{w}_h^0$  is the  $\mathbf{S}_h(0)$ -approximation of  $\boldsymbol{w}^0$ . It means that

$$\left(\boldsymbol{w}_{h}^{0}, \boldsymbol{\varphi}_{h}
ight) = \left(\boldsymbol{w}^{0}, \boldsymbol{\varphi}_{h}
ight) \quad \forall \boldsymbol{\varphi}_{h} \in \mathbf{S}_{h}(0).$$

## 2.2 Time discretization

Let us consider a partition  $0 = t_0 < t_1 < ... < t_M$  of the interval [0, T],  $t_k = k\tau$ ,  $\tau > 0$ . We use the approximation  $\boldsymbol{w}_h(t_l) \approx \boldsymbol{w}_h^l$ , defined in  $\Omega_h(t_l)$ . Then we set  $\hat{\boldsymbol{w}}_h^k(x) = \boldsymbol{w}_h^k(\mathcal{A}_{t_k}(\mathcal{A}_{t_{k+1}}^{-1}(x))), \quad x \in \Omega_h(t_{k+1})$ , and approximate the ALE-derivative using the first order backward difference:

$$\left(\frac{D^{\mathcal{A}}\boldsymbol{w}_{h}(t_{k+1})}{Dt},\boldsymbol{\varphi}_{h}\right) \approx \left(\frac{\boldsymbol{w}_{h}^{k+1}-\hat{\boldsymbol{w}}_{h}^{k}}{\tau},\boldsymbol{\varphi}_{h}\right).$$

Since the terms  $\tilde{a}_h$  and  $\tilde{b}_h$  are nonlinear, we shall linearized them. For  $\tilde{b}_h$  we use the property (3) of  $\boldsymbol{f}_s$  and the definition of  $\boldsymbol{g}_s$ . We get the approximation

$$\sum_{i \in I(t)} \int_{K_i} \sum_{s=1}^2 \boldsymbol{g}_s(\boldsymbol{w}) \cdot \frac{\partial \boldsymbol{\varphi}_h}{\partial x_s} \mathrm{d}x \approx \sigma_1 = \sum_{i \in I(t_{k+1})} \int_{K_i} \sum_{s=1}^2 \left( \mathbf{A}_s(\hat{\boldsymbol{w}}_h^k) - z_s \mathbf{I} \right) \boldsymbol{w}_h^{k+1} \cdot \frac{\partial \boldsymbol{\varphi}_h}{\partial x_s} \mathrm{d}x.$$

Now let us set  $\mathbf{P}(\boldsymbol{w}, \boldsymbol{n}) := \sum_{s=1}^{2} (\mathbf{A}_{s}(\boldsymbol{w}) - z_{s}\mathbf{I}) n_{s}$ ,  $(\boldsymbol{n} = (n_{1}, n_{2}), n_{1}^{2} + n_{2}^{2} = 1)$ . We have  $\sum_{s=1}^{2} \boldsymbol{g}_{s}(\boldsymbol{w})n_{s} = \mathbf{P}(\boldsymbol{w}, \boldsymbol{n})\boldsymbol{w}$ . It is possible to show that the matrix  $\mathbf{P}$  is diagonalizable:  $\mathbf{P} = \mathbf{T}\mathbf{D}\mathbf{T}^{-1}$ , where  $\mathbf{T}$  is a nonsingular matrix,  $\mathbf{D} = \operatorname{diag}(\lambda_{1}, ..., \lambda_{4})$  is a diagonal matrix and  $\lambda_{i}$  are the eigenvalues of  $\mathbf{P}$ . Then we can define the "positive" and "negative" parts of the matrix  $\mathbf{P}: \mathbf{P}^{\pm} = \mathbf{T}\mathbf{D}^{\pm}\mathbf{T}^{-1}$ , where  $\mathbf{D}^{\pm} = \operatorname{diag}(\lambda_{1}^{\pm}, ..., \lambda_{4}^{\pm})$  and  $\lambda^{+} = \max(\lambda, 0), \ \lambda^{-} = \min(\lambda, 0)$ . Using this concept, we introduce the so-called Vijayasundaram numerical flux

$$\mathbf{H}_V(oldsymbol{w}_1,oldsymbol{w}_2,oldsymbol{n}) = \mathbf{P}^+\left(rac{oldsymbol{w}_1+oldsymbol{w}_2}{2},oldsymbol{n}
ight)oldsymbol{w}_1+\mathbf{P}^-\left(rac{oldsymbol{w}_1+oldsymbol{w}_2}{2},oldsymbol{n}
ight)oldsymbol{w}_2.$$

Then we can approximate integrals over faces in the following way:

$$\sum_{i \in I(t)} \sum_{j \in S(i)(t)} \int_{\Gamma_{ij}} \mathbf{H}(\boldsymbol{w}|_{\Gamma_{ij}}, \boldsymbol{w}|_{\Gamma_{ji}}, \boldsymbol{n}_{ij}) \, \mathrm{d}S \approx \sigma_2 :=$$

$$\sum_{i \in I(t_{k+1})} \sum_{j \in S(i)(t_{k+1})} \int_{\Gamma_{ij}} \mathbf{P}^+ \left(\frac{\hat{\boldsymbol{w}}_h^k|_{\Gamma_{ij}} + \hat{\boldsymbol{w}}_h^k|_{\Gamma_{ji}}}{2}, \boldsymbol{n}_{ij}\right) \boldsymbol{w}_h^{k+1}|_{\Gamma_{ij}} \cdot \boldsymbol{\varphi}_h \, \mathrm{d}S$$

$$+ \sum_{i \in I(t_{k+1})} \sum_{j \in S(i)(t_{k+1})} \int_{\Gamma_{ij}} \mathbf{P}^- \left(\frac{\hat{\boldsymbol{w}}_h^k|_{\Gamma_{ij}} + \hat{\boldsymbol{w}}_h^k|_{\Gamma_{ji}}}{2}, \boldsymbol{n}_{ij}\right) \boldsymbol{w}_h^{k+1}|_{\Gamma_{ji}} \cdot \boldsymbol{\varphi}_h \, \mathrm{d}S$$

and define the form  $b_h(\hat{\boldsymbol{w}}_h^k, \boldsymbol{w}_h^{k+1}, \boldsymbol{\varphi}_h) = -\sigma_1 + \sigma_2.$ 

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Using (3), we linearize viscous terms:

$$a_{h}(\hat{\boldsymbol{w}}_{h}^{k}, \boldsymbol{w}_{h}^{k+1}\boldsymbol{\varphi}_{h}) = -\sum_{i \in I(t_{k+1})} \int_{K_{i}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{s,k}(\hat{\boldsymbol{w}}_{h}^{k}) \frac{\partial \boldsymbol{w}_{h}^{k+1}}{\partial x_{k}} \cdot \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{s}} dx$$

$$+ \sum_{i \in I(t_{k+1})} \sum_{j \in s(i)(t_{k+1})} \int_{\Gamma_{ij}} \sum_{s=1}^{2} \left\langle \sum_{k=1}^{2} \mathbf{K}_{s,k}(\hat{\boldsymbol{w}}_{h}^{k}) \frac{\partial \boldsymbol{w}_{h}^{k+1}}{\partial x_{k}} \right\rangle (n_{ij})_{s} \cdot [\boldsymbol{\varphi}_{h}] dS$$

$$+ \sum_{i \in I(t_{k+1})} \sum_{j \in \gamma_{D}(i)(t_{k+1})} \int_{\Gamma_{ij}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{s,k}(\hat{\boldsymbol{w}}_{h}^{k}) \frac{\partial \boldsymbol{w}_{h}^{k+1}}{\partial x_{k}} \left\langle n_{ij} \right\rangle_{s} \cdot \boldsymbol{\varphi}_{h} dS$$

$$+ \Theta \sum_{i \in I(t_{k+1})} \sum_{j \in s(i)(t_{k+1})} \int_{\Gamma_{ij}} \sum_{s=1}^{2} \left\langle \sum_{k=1}^{2} \mathbf{K}_{k,s}^{T}(\hat{\boldsymbol{w}}_{h}^{k}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}} \right\rangle (n_{ij})_{s} \cdot [\boldsymbol{w}_{h}^{k+1}] dS$$

$$+ \Theta \sum_{i \in I(t_{k+1})} \sum_{j \in \gamma_{D}(i)(t_{k+1})} \int_{\Gamma_{ij}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{k,s}^{T}(\hat{\boldsymbol{w}}_{h}^{k}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}} \left\langle n_{ij} \right\rangle_{s} \cdot [\boldsymbol{w}_{h}^{k+1}] dS$$

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and the right-hand side form:

$$l_{h}(\hat{\boldsymbol{w}}_{h}^{k},\boldsymbol{\varphi}_{h}) = \Theta \sum_{i \in I(t_{k+1})} \sum_{j \in \gamma_{D}(i)(t_{k+1})} \int_{\Gamma_{ij}} \sum_{s=1}^{2} \sum_{s=1}^{2} \mathbf{K}_{k,s}^{T}(\hat{\boldsymbol{w}}_{h}^{k}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}}(n_{ij})_{s} \cdot \boldsymbol{w}_{B}^{k+1} \mathrm{d}S$$
$$+ \sum_{i \in I(t_{k+1})} \sum_{j \in \gamma_{D}(i)(t_{k+1})} \int_{\Gamma_{ij}} \frac{C_{W}}{h(\Gamma_{ij})Re} \boldsymbol{w}_{B}^{k+1} \cdot \boldsymbol{\varphi}_{h} \mathrm{d}S$$

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All these considerations lead us to the following semi-implicit scheme: For k = 0, 1, ... find  $\boldsymbol{w}_h^{k+1} \in \mathbf{S}_h(t_{k+1})$  such that

$$\left(\frac{\boldsymbol{w}_{h}^{k+1} - \hat{\boldsymbol{w}}_{h}^{k}}{\tau}, \boldsymbol{\varphi}_{h}\right) - \left(\operatorname{div}\boldsymbol{z}(t_{k+1})\boldsymbol{w}_{h}^{k+1}, \boldsymbol{\varphi}_{h}\right) + b_{h}(\hat{\boldsymbol{w}}_{h}^{k}, \boldsymbol{w}_{h}^{k+1}, \boldsymbol{\varphi}_{h}) \qquad (4)$$

$$+ a_{h}(\hat{\boldsymbol{w}}_{h}^{k}, \boldsymbol{w}_{h}^{k+1}, \boldsymbol{\varphi}_{h}) + J_{h}^{\sigma}(\boldsymbol{w}_{h}^{k+1}, \boldsymbol{\varphi}_{h}) = l_{h}(\hat{\boldsymbol{w}}_{h}^{k}, \boldsymbol{\varphi}_{h}) \quad \forall \boldsymbol{\varphi}_{h} \in \mathbf{S}_{h}(t_{k+1}).$$

## **3** Fluid-structure interaction

We shall simulate motion of a profile with two degrees of freedom: H - displacement of the profile in the vertical direction and  $\alpha$  - the rotation of the profile around the so-called elastic axis. The motion of the profile is described by the system of ordinary differential equations

$$m\ddot{H} + k_{HH}H + S_{\alpha}\ddot{\alpha} = -L(t), \qquad (5)$$
  

$$S_{\alpha}\ddot{H} + I_{\alpha}H + k_{\alpha\alpha}\alpha = M(t),$$

where we use the following notation: m - mass of the airfoil, L(t) - aerodynamic lift force, M(t) - aerodynamic torsional moment,  $S_{\alpha}$  - static moment of the airfoil



**Fig. 1:** Displacement H (left) and rotation angle  $\alpha$  (right) of the airfoil in dependence on time for far-field velocity 10, 30 and 40 m/s.

around the elastic axis,  $I_{\alpha}$  - inertia moment of the airfoil around the elastic axis,  $k_{HH}$  - bending stiffness,  $k_{\alpha\alpha}$  - torsional stiffness. For the derivation of system (5) see, e.g. [5].

System (5) is transformed to a first-order system and solved by the fourth-order Runge-Kutta method together with the discrete flow problem (4). The ALE mapping is constructed on the new time level  $t_{k+1}$  on the basis of the computed values  $H(t_{k+1})$  and  $\alpha(t_{k+1})$ .

#### 4 Numerical experiments

We perform numerical experiments with the following data and initial conditions:  $m = 0.086622 \text{ kg}, S_a = -0.000779673 \text{ kg m}, I_a = 0.000487291 \text{ kg m}^{-2}, k_{HH} = 105.109 \text{ N/m}, k_{\alpha\alpha} = 3.696682 \text{ Nm/rad}, l = 0.05 \text{ m}, c = 0.3 \text{ m}, \text{ far-field density}$  $\rho = 1.225 \text{ kg m}^{-3}, H(0) = -20 \text{ mm}, \alpha(0) = 6^{\circ}, \dot{H}(0) = \dot{\alpha}(0) = 0.$  Figure 1 shows the displacement H and the rotation angle  $\alpha$  in dependence on time for the far-field velocity 10, 30 and 40 m/s. We see that for the velocities 10 and 30 m/s the vibrations are damped, but for the velocity 40 m/s we get the flutter instability when the vibration amplitudes are increasing in time. The monotonous increase and decrease of the average values of H and  $\alpha$ , respectively, shows that the flutter is combined with a divergence instability in the presented example.

These results are qualitatively comparable with vibrations of the airfoil NACA 0012 induced by viscous incompressible flow, contained in [3]. For low far-field velocity the differences of the presented results and results from [3] are small, because the compressibility of the fluid is not significant. For the far-field velocity 40 m/s the qualitative behaviour of the vibrations (flutter combined with divergence) is comparable with the results in [3] obtained by the finite element method. The quantitative difference is already larger probably due to compressibility taken into account in the present paper.

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