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# INTERACTION OF COMPRESSIBLE FLOW WITH AN AIRFOIL* 

Jan Česenek, Miloslav Feistauer


#### Abstract

The paper is concerned with the numerical solution of interaction of compressible flow and a vibrating airfoil with two degrees of freedom, which can rotate around an elastic axis and oscillate in the vertical direction. Compressible flow is described by the Navier-Stokes equations written in the ALE form. This system is discretized by the semi-implicit discontinuous Galerkin finite element method (DGFEM) and coupled with the solution of ordinary differential equations describing the airfoil motion. Computational results showing the flow induced airfoil vibrations are presented.


## 1 Formulation of the continuous problem

We consider 2D compressible viscous flow in a bounded domain $\Omega(t) \subset R^{2}$ depending on time $t \in[0, T]$. We assume that the boundary $\partial \Omega(t)$ of $\Omega(t)$ consists of three disjoint parts: $\partial \Omega(t)=\Gamma_{I} \cup \Gamma_{O} \cup \Gamma_{W}(t)$, where $\Gamma_{I}$ is inlet, $\Gamma_{O}$ is outlet and $\Gamma_{W}(t)$ is impermeable wall, whose part may move.

The time dependence of the domain is taken into account with the aid of a regular one-to-one ALE mapping (cf. [4]) $\mathcal{A}_{t}: \Omega_{0} \longrightarrow \Omega_{t}$, i.e. $\mathcal{A}_{t}: X \longmapsto x=$ $x(X, t)=\mathcal{A}_{t}(X)$. We define the ALE velocity $\tilde{\boldsymbol{z}}(X, t)=\partial \mathcal{A}_{t}(X) / \partial t, \boldsymbol{z}(x, t)=$ $\tilde{\boldsymbol{z}}\left(\mathcal{A}^{-1}(x), t\right), \quad t \in[0, T], X \in \Omega_{0}, x \in \Omega_{t}$, and the ALE derivative of a function $f=f(x, t)$ defined for $x \in \Omega_{t}$ and $t \in(0, T): D^{A} f(x, t) / D t=\partial \tilde{f}(X, t) / \partial t$, where $\tilde{f}(X, t)=f\left(\mathcal{A}_{t}(X), t\right), \quad X \in \Omega_{0}$.

The system describing compressible flow consisting of the continuity equation, the Navier-Stokes equations and the energy equation (see, e.g. [2]) can be written in the ALE form

$$
\begin{equation*}
\frac{D^{A} \boldsymbol{w}}{D t}+\sum_{s=1}^{2} \frac{\partial \boldsymbol{g}_{s}(\boldsymbol{w})}{\partial x_{s}}+\boldsymbol{w} \operatorname{div} \boldsymbol{z}=\sum_{s=1}^{2} \frac{\partial \boldsymbol{R}_{s}(\boldsymbol{w}, \nabla \boldsymbol{w})}{\partial x_{s}} \tag{1}
\end{equation*}
$$

where for $i, j=1,2$ we have

$$
\begin{align*}
& \boldsymbol{w}=\left(w_{1}, \ldots, w_{4}\right)^{T}=\left(\rho, \rho v_{1}, \rho v_{2}, E\right)^{T} \in \mathbb{R}^{4}, \quad \boldsymbol{g}_{i}(\boldsymbol{w})=\boldsymbol{f}_{i}(\boldsymbol{w})-z_{i} \boldsymbol{w},  \tag{2}\\
& \boldsymbol{f}_{i}(\boldsymbol{w})=\left(f_{i 1}, \cdots, f_{i 4}\right)^{T}=\left(\rho v_{i}, \rho v_{1} v_{i}+\delta_{1 i} p, \rho v_{2} v_{i}+\delta_{2 i} p,(E+p) v_{i}\right)^{T}, \\
& \boldsymbol{R}_{i}(\boldsymbol{w}, \nabla \boldsymbol{w})=\left(R_{i 1}, \ldots, R_{i 4}\right)^{T}=\left(0, \tau_{i 1}^{V}, \tau_{i 2}^{V}, \tau_{i 1}^{V} v_{1}+\tau_{i 2}^{V} v_{2}+k \partial \theta / \partial x_{i}\right)^{T}, \\
& \tau_{i j}^{V}=\left(-2 \operatorname{div} \boldsymbol{v} / 3 \delta_{i j}+2 d_{i j}(\boldsymbol{v})\right) / R e, d_{i j}(\boldsymbol{v})=\left(\partial v_{i} / \partial x_{j}+\partial v_{j} / \partial x_{i}\right) / 2 .
\end{align*}
$$

[^0]We use the following notation: $\rho$ - density, $p$ - pressure, $E$ - total energy, $\boldsymbol{v}=$ $\left(v_{1}, v_{2}\right)$ - velocity, $\theta$ - absolute temperature, $\gamma>1$ - Poisson adiabatic constant, $c_{v}>0$ - specific heat at constant volume, $R e$ - the Reynolds number, $k$ - heat conduction. The vector-valued function $\boldsymbol{w}$ is called the state vector, the functions $\boldsymbol{f}_{i}$ are the so-called inviscid fluxes and $\boldsymbol{R}_{i}$ represent viscous terms. The above system is completed by the thermodynamical relations

$$
p=(\gamma-1)\left(E-\rho|\boldsymbol{v}|^{2} / 2\right), \theta=\left(E / \rho-|\boldsymbol{v}|^{2} / 2\right) / c_{v}
$$

and equipped with the initial condition $\boldsymbol{w}(x, 0)=\boldsymbol{w}^{0}(x), x \in \Omega_{0}$, and the following boundary conditions:

$$
\begin{aligned}
& \rho=\rho_{D}, \boldsymbol{v}=\boldsymbol{v}_{D}, \sum_{i, j=1}^{2} \tau_{i j}^{V} n_{i} v_{j}+k \frac{\partial \theta}{\partial n}=0 \text { on } \Gamma_{I}, \\
& \left.\boldsymbol{v}\right|_{\Gamma_{W_{t}}}=\boldsymbol{z}_{D}-\text { velocity of a moving wall, } \partial \theta / \partial n=0 \text { on } \Gamma_{W_{t}}, \\
& \sum_{i=1}^{2} \tau_{i j}^{V} n_{i}=0, j=1,2, \partial \theta / \partial n=0 \text { on } \Gamma_{O},
\end{aligned}
$$

with given data $\boldsymbol{w}^{0}, \rho_{D}, \boldsymbol{v}_{D}, \boldsymbol{z}_{D}$.
The terms $\boldsymbol{R}_{s}$ and $\boldsymbol{f}_{s}$ satisfy the relations
where $\mathbf{K}_{s, k}(\boldsymbol{w}) \in R^{4 \times 4}$ and $\mathbf{A}_{s}$ is the Jacobian matrix of $\boldsymbol{f}_{s}$.

## 2 Discretization

### 2.1 Discontinuous Galerkin space discretization

By $\Omega_{h}(t)$ we denote polygonal approximation of the domain $\Omega(t)$. Let $\mathcal{T}_{h}(t)=$ $\left\{K_{i}\right\}_{i \in I(t)}$ be a triangulation of the domain $\Omega_{h}(t)$ formed by a finite number of closed triangles $K_{i}$ with mutually disjoint interiors. We set $h_{K}=\operatorname{diam}(K)$ as the diameter of $K, h(t)=\max _{K \in \mathcal{T}_{h}(t)} h_{K},|K|$ is the Lebesgue measure of $K$. All elements of $\mathcal{T}_{h}(t)=\left\{K_{i}\right\}_{i \in I(t)}$ will be numbered so that $I(t) \subset Z^{+}=\{0,1,2,3, \ldots\}$ is a suitable index set. If two elements have a common face, than we call them neighbours and put $\Gamma_{i j}=\Gamma_{j i}=\partial K_{i} \cap \partial K_{j}$. For each $i \in I(t)$ we define the index set $s(i)(t)=\left\{j \in I(t) ; K_{j}\right.$ is a neighbour of $\left.K_{i}\right\}$. The boundary $\partial \Omega_{h}(t)$ is formed by a finite number of sides of elements $K_{i}$ adjacent to $\partial \Omega_{h}(t)$. We denote all these boundary sides by $S_{j}$, where $j \in I_{b}(t) \subset Z^{-}=\{-1,-2,-3, \ldots\}$ and set $\gamma(i)(t)=\left\{j \in I_{b}(t) ; S_{j}\right.$ is a side of $\left.K_{i}\right\}, \Gamma_{i j}=S_{j}$ for $K_{i} \in \mathcal{T}_{h}(t)$ such that $S_{j} \subset \partial K_{i}, j \in I_{b}(t)$. For an element $K_{i}$, not containing any boundary side $S_{j}$, we set $\gamma(i)(t)=\emptyset$. Obviously $s(i)(t) \cap \gamma(i)(t)=\emptyset$ for all $i \in I(t)$. Moreover we define $S(i)(t)=s(i)(t) \cup \gamma(i)(t)$.

We shall look for an approximate solution of the problem in the space $\mathbf{S}_{h}(t)=$ $\left\{v ;\left.v\right|_{K} \in P^{r}(K), \forall K \in \mathcal{T}_{h}(t)\right\}^{4}$, where $r \geq 0$ is an integer and $P^{r}(K)$ is the space
of polynomials of degree at most $r$ on $K$. If $v \in \mathbf{S}$, then we use the notation $\left.v\right|_{\Gamma_{i j}}$ and $\left.v\right|_{\Gamma_{j i}}$ for the traces of $v$ on $\Gamma_{i j}$ from the side of the adjacent elements $K_{i}$ and $K_{j}$, respectively, $\langle v\rangle_{\Gamma_{i j}}$ for the average of traces of $v$ on the face $\Gamma_{i j}$ from the side of the adjacent elements and $[v]_{\Gamma_{i j}}$ the jump of $v$ on $\Gamma_{i j}$. By $\boldsymbol{n}_{i j}$ we denote the unit outer normal to the boundary of $K_{i}$ on $\Gamma_{i j}$.

For arbitrary $t \in[0, T]$ we can multiply the system by a test function $\varphi \in \mathbf{S}_{h}(t)$ integrate and sum over all $K_{i} \in \mathcal{T}_{h}(t)$, apply Green's theorem and introduce a numerical flux $\mathbf{H}$. Then we introduce the following forms (cf. [1]):

$$
\begin{aligned}
\tilde{b}_{h}\left(\boldsymbol{w}, \boldsymbol{\varphi}_{h}\right)= & -\sum_{i \in I(t)} \int_{K_{i}} \sum_{s=1}^{2} \boldsymbol{g}_{s}(\boldsymbol{w}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{s}} \mathrm{~d} x+\sum_{i \in I(t)} \sum_{i \in S(i)(t)} \int_{\Gamma_{i j}} \mathbf{H}\left(\left.\boldsymbol{w}\right|_{\Gamma_{i j}},\left.\boldsymbol{w}\right|_{\Gamma_{j i}}, \boldsymbol{n}_{i j}\right) \mathrm{d} S \\
\tilde{a}_{h}\left(\boldsymbol{w}, \boldsymbol{\varphi}_{h}\right)= & -\sum_{i \in I(t)} \int_{K_{i}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{s, k}(\boldsymbol{w}) \frac{\partial \boldsymbol{w}}{\partial x_{k}} \cdot \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{s}} \mathrm{~d} x \\
& +\sum_{i \in I(t)} \sum_{\substack{s \in s(i)(t) \\
j<i}} \int_{\Gamma_{i j}} \sum_{s=1}^{2}\left\langle\sum_{k=1}^{2} \mathbf{K}_{s, k}(\boldsymbol{w}) \frac{\partial \boldsymbol{w}}{\partial x_{k}}\right\rangle\left(n_{i j}\right)_{s} \cdot\left[\boldsymbol{\varphi}_{h}\right] \mathrm{d} S \\
& +\sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{i j}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{s, k}(\boldsymbol{w}) \frac{\partial \boldsymbol{w}}{\partial x_{k}}\left(n_{i j}\right)_{s} \cdot \boldsymbol{\varphi}_{h} \mathrm{~d} S \\
& +\Theta \sum_{i \in I(t)} \sum_{j \in s(i)(t)} \int_{\Gamma_{i j}} \sum_{s=1}^{2}\left\langle\sum_{k=1}^{2} \mathbf{K}_{k, s}^{T}(\boldsymbol{w}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}}\right\rangle\left(n_{i j}\right)_{s} \cdot[\boldsymbol{w}] \mathrm{d} S \\
& +\Theta \sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{i j}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{k, s}^{T}(\boldsymbol{w}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}}\left(n_{i j}\right)_{s} \cdot \boldsymbol{w} \mathrm{~d} S \\
J_{h}^{\sigma}\left(\boldsymbol{w}, \boldsymbol{\varphi}_{h}\right)= & \sum_{i \in I(t)} \sum_{j \in s(i)(t)} \int_{\Gamma_{i j}} \sigma[\boldsymbol{w}] \cdot\left[\boldsymbol{\varphi}_{h}\right] \mathrm{d} S+\sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{i j}} \sigma \boldsymbol{w} \cdot \boldsymbol{\varphi}_{h} \mathrm{~d} S \\
\tilde{l}_{h}\left(\boldsymbol{w}, \boldsymbol{\varphi}_{h}\right)= & \Theta \sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{i j}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{k, s}^{T}(\boldsymbol{w}) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}}\left(n_{i j}\right)_{s} \cdot \boldsymbol{w}_{B} \mathrm{~d} S \\
& +\sum_{i \in I(t)} \sum_{j \in \gamma_{D}(i)(t)} \int_{\Gamma_{i j}} \sigma \boldsymbol{w}_{B} \cdot \boldsymbol{\varphi}_{h} \mathrm{~d} S,
\end{aligned}
$$

where $\left.\sigma\right|_{\Gamma_{i j}}=\frac{C_{W}}{h\left(\Gamma_{i j}\right) R e}, C_{W}>0$ is a suitable sufficiently large constants and $\boldsymbol{w}_{B}$ is a boundary state defined by the Dirichlet boundary condition and extrapolation. By $(\cdot, \cdot)$ we denote the $L^{2}\left(\Omega\left(t_{k+1}\right)\right)$-scalar product. We set $\Theta=-1$ or 0 or 1 and get the so-called nonsymmetric or incomplete or symmetric version of the viscous form. In practical computations we use $\Theta=1$.

Now we can define the discrete problem: Find $\boldsymbol{w}_{h}(t) \in \mathbf{S}_{h}(t)$ such that

$$
\begin{aligned}
& \left(\frac{D^{\mathcal{A}} \boldsymbol{w}_{h}(t)}{D t}, \boldsymbol{\varphi}_{h}\right)-\left(\operatorname{div} \boldsymbol{z}(t) \boldsymbol{w}_{h}(t), \boldsymbol{\varphi}_{h}\right)+\tilde{b}_{h}\left(\boldsymbol{w}_{h}(t), \boldsymbol{\varphi}_{h}\right)+\tilde{a}_{h}\left(\boldsymbol{w}_{h}(t), \boldsymbol{\varphi}_{h}\right) \\
+ & J_{h}^{\sigma}\left(\boldsymbol{w}_{h}(t), \boldsymbol{\varphi}_{h}\right)=\tilde{l}_{h}\left(\boldsymbol{\varphi}_{h}\right) \quad \forall \boldsymbol{\varphi}_{h} \in \mathbf{S}_{h}(t), \quad \forall t \in(0, T), \\
& \boldsymbol{w}_{h}(0)=\boldsymbol{w}_{h}^{0} .
\end{aligned}
$$

where $\boldsymbol{w}_{h}^{0}$ is the $\mathbf{S}_{h}(0)$-approximation of $\boldsymbol{w}^{0}$. It means that

$$
\left(\boldsymbol{w}_{h}^{0}, \boldsymbol{\varphi}_{h}\right)=\left(\boldsymbol{w}^{0}, \boldsymbol{\varphi}_{h}\right) \quad \forall \boldsymbol{\varphi}_{h} \in \mathbf{S}_{h}(0) .
$$

### 2.2 Time discretization

Let us consider a partition $0=t_{0}<t_{1}<\ldots<t_{M}$ of the interval [0,T], $t_{k}=k \tau$, $\tau>0$. We use the approximation $\boldsymbol{w}_{h}\left(t_{l}\right) \approx \boldsymbol{w}_{h}^{l}$, defined in $\Omega_{h}\left(t_{l}\right)$. Then we set $\hat{\boldsymbol{w}}_{h}^{k}(x)=\boldsymbol{w}_{h}^{k}\left(\mathcal{A}_{t_{k}}\left(\mathcal{A}_{t_{k+1}}^{-1}(x)\right)\right), \quad x \in \Omega_{h}\left(t_{k+1}\right)$, and approximate the ALE-derivative using the first order backward difference:

$$
\left(\frac{D^{\mathcal{A}} \boldsymbol{w}_{h}\left(t_{k+1}\right)}{D t}, \boldsymbol{\varphi}_{h}\right) \approx\left(\frac{\boldsymbol{w}_{h}^{k+1}-\hat{\boldsymbol{w}}_{h}^{k}}{\tau}, \boldsymbol{\varphi}_{h}\right) .
$$

Since the terms $\tilde{a}_{h}$ and $\tilde{b}_{h}$ are nonlinear, we shall linearized them. For $\tilde{b}_{h}$ we use the property (3) of $\boldsymbol{f}_{s}$ and the definition of $\boldsymbol{g}_{s}$. We get the approximation

$$
\sum_{i \in I(t)} \int_{K_{i}} \sum_{s=1}^{2} \boldsymbol{g}_{s}(\boldsymbol{w}) \cdot \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{s}} \mathrm{~d} x \approx \sigma_{1}=\sum_{i \in I\left(t_{k+1}\right)} \int_{K_{i}} \sum_{s=1}^{2}\left(\mathbf{A}_{s}\left(\hat{\boldsymbol{w}}_{h}^{k}\right)-z_{s} \mathbf{I}\right) \boldsymbol{w}_{h}^{k+1} \cdot \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{s}} \mathrm{~d} x
$$

Now let us set $\mathbf{P}(\boldsymbol{w}, \boldsymbol{n}):=\sum_{s=1}^{2}\left(\mathbf{A}_{s}(\boldsymbol{w})-z_{s} \mathbf{I}\right) n_{s}, \quad\left(\boldsymbol{n}=\left(n_{1}, n_{2}\right), n_{1}^{2}+n_{2}^{2}=1\right)$. We have $\sum_{s=1}^{2} \boldsymbol{g}_{s}(\boldsymbol{w}) n_{s}=\mathbf{P}(\boldsymbol{w}, \boldsymbol{n}) \boldsymbol{w}$. It is possible to show that the matrix $\mathbf{P}$ is diagonalizable: $\mathbf{P}=\mathbf{T D T}^{\mathbf{- 1}}$, where $\mathbf{T}$ is a nonsingular matrix, $\mathbf{D}=\operatorname{diag}\left(\lambda_{1}, \ldots, \lambda_{4}\right)$ is a diagonal matrix and $\lambda_{i}$ are the eigenvalues of $\mathbf{P}$. Then we can define the "positive" and "negative" parts of the matrix $\mathbf{P}: \mathbf{P}^{ \pm}=\mathbf{T} \mathbf{D}^{ \pm} \mathbf{T}^{\mathbf{- 1}}$, where $\mathbf{D}^{ \pm}=\operatorname{diag}\left(\lambda_{1}^{ \pm}, \ldots, \lambda_{4}^{ \pm}\right)$ and $\lambda^{+}=\max (\lambda, 0), \lambda^{-}=\min (\lambda, 0)$. Using this concept, we introduce the so-called Vijayasundaram numerical flux

$$
\mathbf{H}_{V}\left(\boldsymbol{w}_{1}, \boldsymbol{w}_{2}, \boldsymbol{n}\right)=\mathbf{P}^{+}\left(\frac{\boldsymbol{w}_{1}+\boldsymbol{w}_{2}}{2}, \boldsymbol{n}\right) \boldsymbol{w}_{1}+\mathbf{P}^{-}\left(\frac{\boldsymbol{w}_{1}+\boldsymbol{w}_{2}}{2}, \boldsymbol{n}\right) \boldsymbol{w}_{2}
$$

Then we can approximate integrals over faces in the following way:

$$
\begin{aligned}
& \sum_{i \in I(t)} \sum_{j \in S(i)(t)} \int_{\Gamma_{i j}} \mathbf{H}\left(\left.\boldsymbol{w}\right|_{\Gamma_{i j}},\left.\boldsymbol{w}\right|_{\Gamma_{j i}}, \boldsymbol{n}_{i j}\right) \mathrm{d} S \approx \sigma_{2}:= \\
& \left.\sum_{i \in I\left(t_{k+1}\right)} \sum_{j \in S(i)\left(t_{k+1}\right)} \int_{\Gamma_{i j}} \mathbf{P}^{+}\left(\frac{\left.\hat{\boldsymbol{w}}_{h}^{k}\right|_{\Gamma_{i j}}+\left.\hat{\boldsymbol{w}}_{h}^{k}\right|_{\Gamma_{j i}}}{2}, \boldsymbol{n}_{i j}\right) \boldsymbol{w}_{h}^{k+1}\right|_{\Gamma_{i j}} \cdot \boldsymbol{\varphi}_{h} \mathrm{~d} S \\
+ & \left.\sum_{i \in I\left(t_{k+1}\right)} \sum_{j \in S(i)\left(t_{k+1}\right)} \int_{\Gamma_{i j}} \mathbf{P}^{-}\left(\frac{\left.\hat{\boldsymbol{w}}_{h}^{k}\right|_{\Gamma_{i j}}+\left.\hat{\boldsymbol{w}}_{h}^{k}\right|_{\Gamma_{j i}}}{2}, \boldsymbol{n}_{i j}\right) \boldsymbol{w}_{h}^{k+1}\right|_{\Gamma_{j i}} \cdot \boldsymbol{\varphi}_{h} \mathrm{~d} S
\end{aligned}
$$

and define the form $b_{h}\left(\hat{\boldsymbol{w}}_{h}^{k}, \boldsymbol{w}_{h}^{k+1}, \boldsymbol{\varphi}_{h}\right)=-\sigma_{1}+\sigma_{2}$.

Using (3), we linearize viscous terms:

$$
\begin{aligned}
& a_{h}\left(\hat{\boldsymbol{w}}_{h}^{k}, \boldsymbol{w}_{h}^{k+1} \boldsymbol{\varphi}_{h}\right)=-\sum_{i \in I\left(t_{k+1}\right)} \int_{K_{i}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{s, k}\left(\hat{\boldsymbol{w}}_{h}^{k}\right) \frac{\partial \boldsymbol{w}_{h}^{k+1}}{\partial x_{k}} \cdot \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{s}} \mathrm{~d} x \\
& +\sum_{i \in I\left(t_{k+1}\right)} \sum_{\substack{j \in s(i)\left(t_{k+1}\right) \\
j<i}} \int_{\Gamma_{i j}} \sum_{s=1}^{2}\left\langle\sum_{k=1}^{2} \mathbf{K}_{s, k}\left(\hat{\boldsymbol{w}}_{h}^{k}\right) \frac{\partial \boldsymbol{w}_{h}^{k+1}}{\partial x_{k}}\right\rangle\left(n_{i j}\right)_{s} \cdot\left[\boldsymbol{\varphi}_{h}\right] \mathrm{d} S \\
& +\sum_{i \in I\left(t_{k+1}\right)} \sum_{j \in \gamma_{D}(i)\left(t_{k+1}\right)} \int_{\Gamma_{i j}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{s, k}\left(\hat{\boldsymbol{w}}_{h}^{k}\right) \frac{\partial \boldsymbol{w}_{h}^{k+1}}{\partial x_{k}}\left(n_{i j}\right)_{s} \cdot \boldsymbol{\varphi}_{h} \mathrm{~d} S \\
& +\Theta \sum_{i \in I\left(t_{k+1}\right)} \sum_{\substack{j \in s(i)\left(t_{k+1}\right) \\
j<i}} \int_{\Gamma_{i j}} \sum_{s=1}^{2}\left\langle\sum_{k=1}^{2} \mathbf{K}_{k, s}^{T}\left(\hat{\boldsymbol{w}}_{h}^{k}\right) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}}\right\rangle\left(n_{i j}\right)_{s} \cdot\left[\boldsymbol{w}_{h}^{k+1}\right] \mathrm{d} S \\
& +\Theta \sum_{i \in I\left(t_{k+1}\right)} \sum_{\substack{j \in \gamma_{D}(i)\left(t_{k+1}\right)}} \int_{\Gamma_{i j}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{k, s}^{T}\left(\hat{\boldsymbol{w}}_{h}^{k}\right) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}}\left(n_{i j}\right)_{s} \cdot \boldsymbol{w}_{h}^{k+1} \mathrm{~d} S,
\end{aligned}
$$

and the right-hand side form:

$$
\begin{aligned}
& l_{h}\left(\hat{\boldsymbol{w}}_{h}^{k}, \boldsymbol{\varphi}_{h}\right)=\Theta \sum_{i \in I\left(t_{k+1}\right)} \sum_{j \in \gamma_{D}(i)\left(t_{k+1}\right)} \int_{\Gamma_{i j}} \sum_{s=1}^{2} \sum_{k=1}^{2} \mathbf{K}_{k, s}^{T}\left(\hat{\boldsymbol{w}}_{h}^{k}\right) \frac{\partial \boldsymbol{\varphi}_{h}}{\partial x_{k}}\left(n_{i j}\right)_{s} \cdot \boldsymbol{w}_{B}^{k+1} \mathrm{~d} S \\
& +\sum_{i \in I\left(t_{k+1}\right)} \sum_{j \in \gamma_{D}(i)\left(t_{k+1}\right)} \int_{\Gamma_{i j}} \frac{C_{W}}{h\left(\Gamma_{i j}\right) R e} \boldsymbol{w}_{B}^{k+1} \cdot \boldsymbol{\varphi}_{h} \mathrm{~d} S
\end{aligned}
$$

All these considerations lead us to the following semi-implicit scheme: For $k=0,1, \ldots$ find $\boldsymbol{w}_{h}^{k+1} \in \mathbf{S}_{h}\left(t_{k+1}\right)$ such that

$$
\begin{align*}
& \left(\frac{\boldsymbol{w}_{h}^{k+1}-\hat{\boldsymbol{w}}_{h}^{k}}{\tau}, \boldsymbol{\varphi}_{h}\right)-\left(\operatorname{div} \boldsymbol{z}\left(t_{k+1}\right) \boldsymbol{w}_{h}^{k+1}, \boldsymbol{\varphi}_{h}\right)+b_{h}\left(\hat{\boldsymbol{w}}_{h}^{k}, \boldsymbol{w}_{h}^{k+1}, \boldsymbol{\varphi}_{h}\right)  \tag{4}\\
& +a_{h}\left(\hat{\boldsymbol{w}}_{h}^{k}, \boldsymbol{w}_{h}^{k+1}, \boldsymbol{\varphi}_{h}\right)+J_{h}^{\sigma}\left(\boldsymbol{w}_{h}^{k+1}, \boldsymbol{\varphi}_{h}\right)=l_{h}\left(\hat{\boldsymbol{w}}_{h}^{k}, \boldsymbol{\varphi}_{h}\right) \quad \forall \boldsymbol{\varphi}_{h} \in \mathbf{S}_{h}\left(t_{k+1}\right) .
\end{align*}
$$

## 3 Fluid-structure interaction

We shall simulate motion of a profile with two degrees of freedom: $H$ - displacement of the profile in the vertical direction and $\alpha$ - the rotation of the profile around the so-called elastic axis. The motion of the profile is described by the system of ordinary differential equations

$$
\begin{align*}
m \ddot{H}+k_{H H} H+S_{\alpha} \ddot{\alpha} & =-L(t)  \tag{5}\\
S_{\alpha} \ddot{H}+I_{\alpha} H+k_{\alpha \alpha} \alpha & =M(t)
\end{align*}
$$

where we use the following notation: $m$ - mass of the airfoil, $L(t)$ - aerodynamic lift force, $M(t)$ - aerodynamic torsional moment, $S_{\alpha}$ - static moment of the airfoil


Fig. 1: Displacement $H$ (left) and rotation angle $\alpha$ (right) of the airfoil in dependence on time for far-field velocity 10, 30 and $40 \mathrm{~m} / \mathrm{s}$.
around the elastic axis, $I_{\alpha}$ - inertia moment of the airfoil around the elastic axis, $k_{H H}$ - bending stiffness, $k_{\alpha \alpha}$ - torsional stiffness. For the derivation of system (5) see, e.g. [5].

System (5) is transformed to a first-order system and solved by the fourth-order Runge-Kutta method together with the discrete flow problem (4). The ALE mapping is constructed on the new time level $t_{k+1}$ on the basis of the computed values $H\left(t_{k+1}\right)$ and $\alpha\left(t_{k+1}\right)$.

## 4 Numerical experiments

We perform numerical experiments with the following data and initial conditions: $m=0.086622 \mathrm{~kg}, S_{a}=-0.000779673 \mathrm{~kg} \mathrm{~m}, I_{a}=0.000487291 \mathrm{~kg} \mathrm{~m}^{-2}, k_{H H}=$ $105.109 \mathrm{~N} / \mathrm{m}, k_{\alpha \alpha}=3.696682 \mathrm{Nm} / \mathrm{rad}, l=0.05 \mathrm{~m}, c=0.3 \mathrm{~m}$, far-field density $\rho=1.225 \mathrm{~kg} \mathrm{~m}^{-3}, H(0)=-20 \mathrm{~mm}, \alpha(0)=6^{\circ}, \dot{H}(0)=\dot{\alpha}(0)=0$.

Figure 1 shows the displacement $H$ and the rotation angle $\alpha$ in dependence on time for the far-field velocity 10,30 and $40 \mathrm{~m} / \mathrm{s}$. We see that for the velocities 10 and $30 \mathrm{~m} / \mathrm{s}$ the vibrations are damped, but for the velocity $40 \mathrm{~m} / \mathrm{s}$ we get the flutter instability when the vibration amplitudes are increasing in time. The monotonous increase and decrease of the average values of $H$ and $\alpha$, respectively, shows that the flutter is combined with a divergence instability in the presented example.

These results are qualitatively comparable with vibrations of the airfoil NACA 0012 induced by viscous incompressible flow, contained in [3]. For low far-field velocity the differences of the presented results and results from [3] are small, because the compressibility of the fluid is not significant. For the far-field velocity $40 \mathrm{~m} / \mathrm{s}$ the qualitative behaviour of the vibrations (flutter combined with divergence) is comparable with the results in [3] obtained by the finite element method. The quantitative difference is already larger probably due to compressibility taken into account in the present paper.

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